

### Interconnection System Impact Study Report REQUEST # GI-2003-1

### 300 MW Generation Addition Near Brush, Colorado Interconnecting at Pawnee Station

#### Xcel Energy Transmission Planning October 2004

#### Executive Summary

This Interconnection System Impact Study Report summarizes the analyses performed by the Transmission Planning group of Public Service Company of Colorado (PSCo) to interconnect 300 MW of wind powered generation (200 1.5 MW units) located near Brush, Colorado to the Pawnee Station 230 kV bus. The Customer proposed in-service date for commercial operation of the 300 MW facility is December 1, 2006, with a backfeed date of June 1, 2006. At the request of the Customer, the Project was evaluated as both an Energy Resource (ER) and as a Network Resource (NR) with the power going to PSCo customers.

#### Energy Resource:

As an Energy Resource, an interconnected generator is only eligible to deliver on an "as available" basis using the existing capacity of the transmission system. This study indicated that the proposed project could inject up to 50 MW at Pawnee Station without requiring any additional Network Upgrades, depending on regional generation patterns and TOT 3 path flow. The estimated cost of the PSCo Network Upgrades associated with an Interconnection for an Energy Resource is \$730,000. The time frame to get the interconnection constructed for the generation addition would be approximately 9 months from the signing of an Interconnection Agreement (IA).

#### Network Resource:

For the Project to be considered a Network Resource, studies indicate that the integration of the full 300 MW of new generation would require transmission additions and modifications in order to prevent unacceptable conditions on the regional system. The estimated cost for Network Upgrades associated with delivery is \$44.7 Million. Therefore, the total estimated cost of the Network Upgrades associated with the interconnection and delivery of the 300 MW facility is \$45.4 Million and the estimated time frame to construct those upgrades is a minimum of 27 months from the signing of the IA.

A simple diagram of the Network Upgrades and the regional transmission system for this request is shown in Figure 1.



#### Introduction

On October 21, 2003 Xcel Energy Transmission received a request to conduct a feasibility study that would evaluate the integration of a 300 MW wind power generating facility in Morgan County, Colorado. The approximate location of the interconnection is approximately 9 miles northwest of the town of Brush, Colorado. The Customer proposed in-service date for commercial operation of the facility is December 1, 2006,

with a back-feed date of June 1, 2006. The Feasibility Study was completed and the report issued to the Customer and posted on the RMAO web site in March 2004. An Interconnection System Impact Study Agreement was executed on or around April 21, 2004 indicating a targeted completion date for studies of 120 days from that date.

#### Study Scope and Analysis

The Interconnection System Impact Study evaluated the transmission requirements associated with the proposed interconnection to the PSCo Transmission System. As per section 7.3 of the FERC LGIP, the Study considered the Base Case as well as all Generating Facilities (and with respect to (iii), any identified Network Upgrades) that, on the date the Interconnection Feasibility Study is commenced:

- (i) are directly interconnected to the Transmission System;
- (ii) are interconnected to Affected Systems and may have an impact on the Interconnection Request;
- (iii) that have a pending higher queued Interconnection Request to interconnect to the Transmission System; and
- (iv) have no Queue Position but have executed an LGIA or requested that an unexecuted LGIA be filed with FERC.

For this study, there were no higher queued requests to consider.

The Study consisted of power flow, short circuit, and dynamic stability analyses. The power flow analysis provided an identification of any thermal or voltage limit violations resulting for the interconnection, and for the NR request, a preliminary identification of Network Upgrades required to deliver the proposed generation to PSCo loads. The short circuit analysis provided a preliminary identification of any circuit breaker short circuit capability limits exceeded as a result of the Interconnection and for the NR request, the delivery of the proposed generation to PSCo loads. The dynamic stability analysis verified that there were no limitations due to angular instability of the system for regional disturbances.

PSCo adheres to NERC / WECC Reliability Criteria, as well as internal Company criteria for planning studies. During system intact conditions, criteria are to maintain transmission system bus voltages between 0.95 and 1.05 per-unit of system normal conditions, and steady state power flows within 1.0 per-unit of all elements thermal (continuous current or MVA) ratings. Operationally, PSCo tries to maintain a transmission system voltage profile ranging from 1.02 per-unit or higher at generation buses, to 1.0 per-unit or higher at transmission load buses. Following a single contingency element outage, transmission system steady state bus voltages must remain within 0.90 per-unit to 1.10 per-unit, and power flows within 1.0 per-unit of the elements continuous thermal ratings.

#### Powerflow Study Models

For this analysis, a power flow model was developed to reflect 2006 heavy summer loading conditions. Data representation in the area of study was reviewed and modified to accurately reflect the Rocky Mountain regional transmission system. The TOT 3

transfer path was increased to a high level of over 1500 MW, and power transfers from north to south through Colorado were increased to study the regional transmission system<sup>1</sup>.

The proposed project was modeled as two 150 MW units. The specified point of interconnection for the new generation is Pawnee Station near Brush, Colorado. The proposed project was connected to the Pawnee Station 230 kV bus with a single 230kV line, approximately 18 miles long. As an NR request, the proposed generation was scheduled to PSCo peaking units located in and around Denver.

#### Study Results

#### Power Flow Analysis

At the request of the Customer, the Project was evaluated as both a Network Resource (NR) and as an Energy Resource (ER) with the power going to PSCo customers.

#### Energy Resource

Two cases were developed to model the TOT 3 transfer path at a two different flow levels. For the first case, with TOT 3 at 1540 MW, results showed that the wind project could not inject any amount of power into the PSCo transmission system unless additional Network Upgrades are constructed. The other case modeled the TOT 3 flow at 1145 MW. At that level, results indicated that the project could inject 50 MW into the PSCo system. Therefore, the amount that the wind project can inject into the PSCo is directly related to the loading of the TOT 3 interface. Contingency results for the ER analysis are shown in Table 1.

<sup>&</sup>lt;sup>1</sup> High north to south transfers are generally used to analyze the transmission system between Pawnee and Denver. The Tot 3 transfer path was modeled at approximately 1535 MW. The 2004 summer transfer limit for that path is approximately 1540 MW.

				-kv-	115	115	345	230	230
			TO BUS	name	BEAVERCK	FMWEST	LAR.RIVR	PLNENDSS	QUINCY
			I	#	73020	73379	73108	70570	70343
			1	-kv-	115	115	345	230	230
		CONTINGENCY	FROM BUS	name	B.CK PS	EFMORGTP	AULT	LOOKOUT	PAWNEE
				#	73013	73305	73012	70266	70311
	Case: 06c1a.say; TOT 3 =1145 MW Case: 06c1a.say; TOT 3 =1145 MW Case: 06c1.say; TOT 3 =1145 MW TOT 7=363 MW, BRUSH WIND @ 50 MW		cont cont	load load	97% 100%	98% 99%	99% 100%	100% 100%	90% 94%
	CASE		rating	[MVA]	200	109	400	280	413.5
			1	D	-	-	<del></del>	۲	1
;				-kv- ID	115 1	115 1	230 1	230 1	230 1
;			TO BUS	namekv- ID	BEAVERCK 115 1	ADENA 115 1	STEGALL 230 1	VALMONT 230 1	PAWNEE 230 1
;			TO BUS	#namekv- ID	73020 BEAVERCK 115 1	73464 ADENA 115 1	73190 STEGALL 230 1	70447 VALMONT 230 1	70311 PAWNEE 230 1
;			TO BUS	zon #namekv- ID	752 73020 BEAVERCK 115 1	752 73464 ADENA 115 1	753 73190 STEGALL 230 1	703 70447 VALMONT 230 1	706 70311 PAWNEE 230 1
;			TO BUS	-kv- zon #namekv- ID	115 752 73020 BEAVERCK 115 1	115 752 73464 ADENA 115 1	230 753 73190 STEGALL 230 1	115 703 70447 VALMONT 230 1	230 706 70311 PAWNEE 230 1
5		DADED ELEMENT	FROM BUS TO BUS	namekv- zon #namekv- ID	B.CK TRI 115 752 73020 BEAVERCK 115 1	BEAVERCK 115 752 73464 ADENA 115 1	ARCHER 230 753 73190 STEGALL 230 1	VALMONT         115         703         70447         VALMONT         230         1	FTLUPTON 230 706 70311 PAWNEE 230 1

Table 1 Power Flow Contingency Results for Energy Resource

As shown above in Table 1, the 50 MW injection limit was established by modeling heavy north to south flows in the region and a mid-level flow on TOT 3. The limiting contingency was an outage of the PSCo 115 kV line from PSCo's Beaver Creek Substation to Western's Beaver Creek Substation. That contingency loaded the parallel Tri-State Beaver Creek 115 kV line to 100% of its flow limit (case 06c1 in Table 1). Higher TOT 3 flows will result in lower delivery capability.

#### Network Resource

By modeling the proposed project at 300 MW and a high TOT 3 flow of 1535 MW, studies revealed contingency overloads. Some sensitivity studies were performed to analyze other generation dispatch scenarios and those scenarios revealed similar contingency overloads. A table of contingency results is provided in Appendix B. To alleviate the overloads and accommodate the full 300 MW of generation, the following upgrades were required:

- Between Pawnee Station and Smoky Hill Substation, uprate the existing 230 kV line from 500 MVA to 800 MVA by using phase raisers to raise 15 transmission structures.
- From Pawnee Station to Ft. Lupton Station rebuild the existing 64 mile 230 kV 413 MVA rated line to a double circuit 230 kV, 800 MVA per circuit configuration.
- Uprate the existing 230 kV line from Story to Pawnee Station from 576 MVA to 650 MVA by adjusting the rating methodology for that line to allow for a higher conductor temperature.
- Uprate the existing 230 kV line from Ft. Lupton Station to Henry Lake Substation to Riverdale Substation to Cherokee Station from 435 MVA to 475 MVA. This can be accomplished by replacing transmission line and equipment jumpers at Riverdale and Cherokee. The 230 kV main buses at Cherokee must also be replaced with 5-inch aluminum bus tube from the existing 1272 kCMIL ACSR.

#### TOT 3 Analysis

TOT 3 analysis was performed by the Western Area Power Administration (Western). The results show that integrating the Brush 300 MW Wind Farm with the transmission infrastructure required for delivery will not have any adverse impact on the TOT 3 limit. The detailed report on the analysis of TOT 3 is available upon request.

#### Short Circuit Study Results

The short circuit analysis consisted of faulting and measuring the current at 230kV buses in the region of study. Three-phase and single-line to ground faults were evaluated and the three-phase faults were found to be more severe. The results are shown in Tables 2, 3, and 4. Results indicated that there are not any major increases in fault currents and that current breaker ratings are sufficient to integrate this project into the PSCo system. Plots and detailed analysis are available upon request

Fault	Description	Fault Current (kA, RMS)				
		1 cycle	3 cycles	6 cycles		
2	LLLG Fault at Fort Lupton 230	25.95	24.34	22.38		
3	LLLG Fault at Story 230	13.80	12.72	11.57		
4	LLLG Fault at Daniel Park 230	27.15	26.93	26.71		
5	LLLG Fault at Quincy 230	13.43	13.25	13.14		
6	LLLG Fault at Pawnee 230	16.86	14.97	10.85		
8	SLG Fault at Fort Lupton 230	18.41	18.34	18.04		
9	SLG Fault at Story 230	11.73	11.50	11.32		
10	SLG Fault at Daniel Park 230	25.78	25.52	25.42		
11	SLG Fault at Quincy 230	9.65	9.47	9.40		
12	SLG Fault at Pawnee 230	19.21	18.39	16.75		

#### Table 2

Table 2: PSCAD Short Circuit Study Results (Case 1: Base Case, no network upgrades and Brush Wind not in service)

Fault	Description	Fault Current (kA, RMS)				
		1 cycle	3 cycles	6 cycles		
1	LLLG Fault at Brushwind 230	8.68	7.80	6.28		
2	LLLG Fault at Fort Lupton 230	25.23	23.96	22.00		
3	LLLG Fault at Story 230	13.41	12.77	10.96		
4	LLLG Fault at Daniel Park 230	27.24	26.62	26.53		
5	LLLG Fault at Quincy 230	13.37	13.13	13.01		
6	LLLG Fault at Pawnee 230	16.68	14.23	9.36		
7	SLG Fault at Brushwind 230	7.29	7.18	7.02		
8	SLG Fault at Fort Lupton 230	18.62	18.17	17.88		
9	SLG Fault at Story 230	12.03	11.76	11.43		
10	SLG Fault at Daniel Park 230	25.78	25.37	25.32		
11	SLG Fault at Quincy 230	9.55	9.33	9.32		
12	SLG Fault at Pawnee 230	19.64	18.47	16.49		

#### Table 3

Table 3: PSCAD Short Circuit Study Results (Case 2: No Network Upgrades and 300MW Brush Windfarm in Service)

Fault	Description	Description Fault Current (kA, RMS)				
		1 cycle 3 cycles		6 cycles		
1	LLLG Fault at Brush wind 230	8.94	8.11	6.90		
2	LLLG Fault at Fort Lupton 230	26.32	24.88	22.62		
3	LLLG Fault at Story 230	13.43	12.57	11.27		
4	LLLG Fault at Daniel Park 230	26.62	26.10	25.77		
5	LLLG Fault at Quincy 230	13.44	13.18	13.01		
6	LLLG Fault at Pawnee 230	17.71	15.33	10.73		
7	SLG Fault at Brush wind 230	7.44	7.31	7.17		
8	SLG Fault at Fort Lupton 230	19.71	19.24	18.93		
9	SLG Fault at Story 230	11.95	11.53	11.34		
10	SLG Fault at Daniel Park 230	25.38	24.94	24.84		
11	SLG Fault at Quincy 230	9.63	9.38	9.36		
12	SLG Fault at Pawnee 230	20.84	19.72	17.92		

#### Table 4



#### **Stability Study Results**

Transient stability analysis of the Pawnee area was performed by modeling three-phase faults and single line to ground fault contingencies in the region of study. The three-phase faults were cleared and elements removed after six cycles. Dynamic models for the proposed project were prepared using Customer supplied data. The analysis indicated that the project would not adversely affect the transient stability performance of the system and results met WECC/NERC Reliability Criteria and that the system is stable before, during, and after contingencies. The disturbances modeled are shown in Table 5. Plots of the stability analysis are available upon request.

#### **TOT 3 Analysis**

Western performed TOT 3 stability analysis by modeling a three-phase fault at the Laramie River 345-kV bus and loss of the Laramie River to Ault 345 kV line. The results showed that the 300 MW wind farm addition, with the proposed network resource additions does not adversely impact the transient performance in the region of the TOT 3 path. These results are shown in Table 5a. Plots of the TOT 3 stability analysis are available upon request.

Fault	Transient Stability Fault List F		Rue To	Fault Cases		
Fault			Dus To	Case 1	Case 2	Case 3
S1	3-Phase Fault midway between Brushwind and Pawnee; Clear after 6 cycles	70600	70311	N/A	<sup>°</sup> Wind Farm Trip	<sup>°</sup> Wind Farm Trip
82	3-Phase Fault midway between Story and Pawnee; Clear after 6 cycles	73192	70311	No Trip	⁺Wind Farm Trip	⁺Wind Farm Trip
83	3-Phase Fault midway between Fort Lupton and Pawnee; Clear after 6 cycles	70192	70311	No Trip	No Trip	No Trip
S4	3-Phase Fault midway between Daniel Park and Pawnee; Clear after 6 cycles	70139	70311	No Trip	No Trip	No Trip
85	3-Phase Fault midway between Pawnee and Quincy (one cct); Clear after 6 cycles	70311	70343	No Trip	No Trip	No Trip
<b>S</b> 6	3-Phase Fault at Pawnee 22kV Bus; Generator trip or disconnect after 3 cycles	70311	-	No Trip	No Trip	No Trip
S7	Sudden Loss of Power due to Wind Gust at new Brushwind Site	-	-	N/A	No Trip	No Trip

#### **Table 5 Summary of Transient Stability Results**

<sup>+</sup> Wind Farm Trips on dV = -0.7 pu, no LVRT; Machine bus voltage remains above 0.15pu

\* Wind Farm Trips on dV = -0.7 pu, no LVRT; Machine bus voltage falls to zero

The transient stability cases are as follows:

Case 1 is the base case before the wind project is added.

Case 2 has the wind project and without any required delivery infrastructure. Case 3 has the wind project and the required delivery infrastructure.

 Table 5a Summary of Transient Stability Results for TOT 3

Fault Location	Open	From Bus	To Bus	Case	Result
3-phase at LRS 345	Open LRS-Ault 345 kV	73108	73012	Base Case without Generation Addition	System Stable Volt Dip at Laramie 115 kV to 0.67 p.u
3-phase at LRS 345	Open LRS-Ault 345 kV	73108	73012	Paw-Ft Lupt double Ckt 230 kV Added.	System Stable Volt Dip at Laramie 115 kV to 0.74 p.u.
3-phase at LRS 345	Open LRS-Ault 345 kV	73108	73012	Wind Farm and Paw- Ft. Lupt. Dbl Ckt added.	System Stable Volt Dip at Laramie 115 kV to 0.72 p.u.

#### Cost Estimates and Assumptions

The estimated costs shown are "indicative" (+/-30%) preliminary budgetary costs in 2006 dollars and are based upon typical construction costs for previously performed similar construction. These estimated costs include all applicable labor and overheads associated with the engineering, design, and construction of these new PSCo facilities. The estimates do not include any costs for any Customer-owned, supplied, and installed equipment and associated design and engineering, other than the transmission line

between the generation and Corner Point. This estimate also does not include any costs that may, or may not be required for other entities' systems. The cost responsibilities associated with these facilities shall be handled as per current FERC guidelines

Based upon the System Impact Study performed here, in order for PSCo to provide an interconnection for the Customer, facilities must be constructed at the PSCo Pawnee Station.

#### **PSCo Network Upgrades for Interconnection:**

Table 6 describes the costs associated with providing an interconnection to PSCo's system. It does not include all of the costs required for full delivery of the generation. Those costs are included in Table 7.

#### Table 6 PSCo Network Upgrades Required for Interconnection

PSCo Interconnection Facilities

Substation	Description	Cost
Pawnee Generation Station	<ul> <li>Interconnect Customer's 230 kV line, which will require the relocation of the existing Pawnee to Story 230 kV line to one bay west to allow the new Customer owned line to terminate in this position. The new equipment required includes:</li> <li>a new 230 kV 3000 A, 50 kA circuit breaker</li> <li>230 kV bi-directional revenue metering</li> <li>two 230 kV switches</li> <li>required steel supporting structures</li> <li>associated control and relaying changes and additions.</li> <li>(See one-line in Appendix D)</li> </ul>	\$660k
	1. Transmission line relocation	\$50k
	2. Siting and Land Rights for misc. permits	\$20k
	3. Total Cost	\$730k

# PSCo Network Upgrades required to deliver the proposed 300 MW as an NR Request:

Table 7 lists the costs associated with developing the transmission system in order to deliver the full 300 MW of generation. The cost of the Network Delivery facilities is the additional change in cost between Interconnection and Delivery.

Table 7 PSCo N	Network Upgrades	<b>Required for</b>	<b>Power Delivery</b>
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	Description	Cost
Pawnee	New 230 kV Line terminal to Ft. Lupton	\$1,430k
Station	requiring the following equipment:	

	<ul> <li>one new 230 kV breaker and half bay on the west side of the 230 kV switch yard</li> <li>two (2) 3000 Amp, 50 kA circuit breakers</li> <li>four (4) 230 kV switches</li> <li>associated steel</li> <li>electrical bus work</li> <li>associated metering, control, and relaying</li> <li>Uprate the 230 kV line from Pawnee to Story requires the following:</li> <li>replace four (4) 230 kV 1600 Amp switches with 3000 Amp switches</li> <li>Uprate the Pawnee to Smoky Hill 230 kV line requires the following:</li> <li>replace six (6) 1600 Amp switches with 3000 Amp switches</li> <li>replace 1200 Amp Line trap with 2000 Amp Line Trap</li> </ul>	
Ft. Lupton Station	<ul> <li>New 230 kV 2000 Amp Line Terminal to Pawnee which will require rearranging of the existing line terminations for the Henry Lake and Green Valley lines. The following equipment will be required: <ul> <li>a new 230 kV breaker and a half bay on the east side of the station</li> <li>three (3) 230 kV 3000 Amp 50 kA circuit breakers that includes replacing one 1600 Amp breaker</li> <li>ten (10) 230 kV switches that includes four (4) new and six (6) replacements from 1600 Amp to 3000 Amp</li> <li>misc. supporting steel</li> <li>electrical bus work</li> <li>associated metering control and relaying</li> </ul> </li> </ul>	\$1,400k
Smoky Hill Substation	<ul> <li>Upgrade existing facilities on the Pawnee 230</li> <li>kV line terminal which includes the following:</li> <li>replace two (2) underrated 230 kV 1600</li> <li>Amp circuit breakers with new 3000 Amp 50 kA circuit breakers</li> <li>replace four (4) 1600 Amp switches with 3000 Amp switches</li> <li>replace 1200 Amp Line trap with 2000</li> <li>Amp Line Trap</li> <li>replace existing east and west main 1272</li> </ul>	\$1,060k

	<ul><li>kCMIL strain buses with 5" aluminum tube bus</li><li>associated metering, control, and relaying</li></ul>	
Riverdale	Replace equipment jumpers and transmission line jumpers.	\$65k
Quinau	Perlage evicting 1200 American runters with	@040k
Substation	2000 Amp line rupters	\$310K
Cherokee	<ul> <li>Replace existing equipment jumpers and transmission line jumpers with (2) 1272 kCMIL ACSR,</li> <li>replace existing north and south 1272 kCMIL ACSR strain bus with 5" aluminum tube bus</li> <li>Replace one 1600 Amp circuit breaker with a 3000 Amp 50 kA breaker</li> </ul>	\$720k
	-	
Transmission	Rebuild existing 413 MVA 230 kV line from Pawnee to Ft. Lupton with new double circuit 230 kV 834 MVA transmission utilizing existing ROW as much as possible	\$38,700k
	Uprate the existing Pawnee to Quincy/Smoky Hill 230kV Line to 800 MVA from 500 MVA by installing approximately 15 phase raisers.	\$210k
	Uprate Ft. Lupton to Henry Lake to Riverdale to Cherokee 230 kV line from 435 MVA to 475 MVA. Need an aerial survey to determine current ground clearances.	\$190k
	Uprate Story to Pawnee 230 kV line from 576 MVA to 650 MVA	\$0
0.11		<b>*</b> 0.4.01
Permitting	obtain necessary siting, permits, and ROW as required	\$610k
	TOTAL COST	\$44,685k
Time Frame		27 Months

# Total costs for Network Upgrades for Interconnection and Delivery Costs = \$45,425,000

### Major Assumptions for Cost Estimates

1. PSCo (or its contractor) crews will perform all construction and wiring associated with PSCo-owned and maintained equipment.

- 2. A Certificate for Convenience and Public Necessity (CCPN) will be required for the transmission line.
- 3. Any NEPA requirements imposed on transmission because of the generation addition will most likely have adverse effects on schedule and deliverables.
- 4. No screening has been estimated at any of the substations. If this is required the cost will be significant at each location.
- 5. Detailed field investigations (surveys, etc.) have not been conducted and could increase these estimates.
- 6. Approximately 5 miles of new transmission line ROW acquisition is assumed for Network Delivery related facilities, since existing ROW will be utilized. The Customer Interconnection requires new ROW.
- 7. These estimates do not include any cost for legal fees.
- 8. All necessary transmission line outages can be obtained. If not, construction duration times will be longer.
- 9. All cost estimates have been escalated to reflect the appropriate year of project activity.

The overall timeline to complete all required transmission and substation facilities is expected to require a minimum of 27 months. If there are problems with local and state approvals, this could require an additional year.

## APPENDIX A PSCo Generation Interconnection Request Queue

#### GENERATION INTERCONNECTION REQUESTS September 1, 2004

Queue Number	Date Received	Generation Type	Service Type	Location County/State	Interconnection Point Station or Line	Net Plant Max MW Sum   Win	In-Service Date	Comments/Status/Reason not Completed
GI-2003-1	10/21/2003	Wind	Network Resource	Morgan Co., CO	Pawnee Substation	300 300	12/1/2006	Feasibility Study complete System Impact Study underway
GI-2003-2	11/3/2003	Coal	Network +Energy Resource	Elbert Co., CO	Smokey Hill- Pawnee 230kV line	500 500	6/1/2008	Feasibility Study complete System Impact Study complete Facilities Study underway
GI-2003-3	11/7/2003	Coal	Network Resource	Pueblo Co., CO	Comanche Substation	750 750	10/1/2009	Feasibility Study complete System Impact Study complete Facilities Study underway
GI-2003-4	11/11/2003	Wind	Network +Energy Resource	Laramie Co., WY	Ponnequin Substation	30 30	Q2:2004	Feasibility Study complete System Impact Study complete
GI-2003-5	12/29/2003	Coal	Network Resource	Morgan Co., CO	Pawnee Substation	750 750	10/1/2009	Request withdrawn 2/20/04
GI-2004-1	1/19/2004	Wind	Network +Energy Resource	Morgan Co., CO	Pawnee Substation	150 150	12/31/2005	Feasibility Study complete
GI-2004-2	2/9/2004	Wind	Network +Energy Resource	Baca Co., CO	Lamar Substation	238 238	9/31/2005	Feasibility Study complete
GI-2004-3	7/16/2004	Wind	Network +Energy Resource	Weld Co., CO	Ault Substation	275 275	12/31/2006	Feasibility Study underway
GI-2004-4	8/9/2004	Wind	Network +Energy Resource	Prowers Co., CO	Lamar Substation	280 280	12/31/2006	
GI-2004-5	8/16/2004 9:05am	Wind	Network +Energy Resource	Weld Co., CO	Fort St. Vrain- Green Valley 230kV Line	402 402	12/30/2006	

GI-2004-6	8/16/2004 9:05am	Wind	Network +Energy Resource	Washington Co., CO	Story Substation	250	250	12/30/2006	
GI-2004-7	8/20/2004 10:25am	Wind	Network +Energy Resource	Elbert Co., CO	Midway-Daniels Park 230kV Line	200	200	12/1/2006	

# **APPENDIX B**

# **POWER FLOW CONTINGENCY RESULTS**

		-kv-	115	230	345	345	345	345	345	345	345	345	345	345	345	345	345	345	345	345	115
		name	ADENA	QUINCY	LAR.RIVR	LAR.RIVR	LAR.RIVR	<b>BEAVERCK</b>													
	To	3US #	3464	0343	3108	3108	3108	3108	3108	3108	3108	3108	3108	3108	3108	3108	3108	3108	3108	3108	3020
		kv- E	115 7	230 7	345 7	345 7	345 7	345 7	345 7	345 7	345 7	345 7	345 7	345 7	345 7	345 7	345 7	345 7	345 7	345 7	115 7
	۲	•					(.)			(,)				(.)							
	CONTINGENC	name	BEAVERCK	PAWNEE	AULT	AULT	AULT	B.CK PS													
	From	BUS #	73020	70311	73012	73012	73012	73012	73012	73012	73012	73012	73012	73012	73012	73012	73012	73012	73012	73012	73013
		Cnt #	245	129	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	234
Base Case (6b-r1.sav) TOT 3=1470 (6b-r1.sav) TOT 7 = 592	cont	load	114%	%66	86%	121%	117%	111%	95%	98%	93%	98%	95%	86%	93%	95%	101%	101%	98%	%06>	107%
Base with 300 WW Wind Base With 300 WW W1541 = 5 TOT (vsz.r1-96) TOT 7 = 621 WW	cont	load	128%	123%	118%	136%	122%	126%	%06>	109%	67%	109%	107%	106%	106%	105%	105%	104%	101%	105%	122%
300 MW  with 2 Paw-Ft. Lup ines TOT3=1455 MW, TOT7=525 MW, (06-fix-r1.sav)	cont	load	107%	%06>	~06>	110%	110%	~06>	105%	%06>	~06>	~06>	~06>	~06>	~06>	%96	94%	93%	%06	~06>	100%
300 MW with 2 Paw-Ft. Lup lines, TOT 3 = 1530 MW TOT7 = 572 MW, (06-fix.sav)	cont	load	109%	%06>	%06>	113%	118%	94%	113%	92%	93%	~06>	~06>	~06>	%06>	93%	100%	100%	~00%	~00%	101%
base with 300 MM ind WM 7131 = 15TOT (vss.93) WM 873 = 7 TOT	cont	load	130%	126%	%06>	132%	125%	122%	%06>	106%	105%	106%	104%	102%	104%	DNS	110%	110%	107%	%06>	124%
TOLL=€34 MM; (€D.53V) TOL 3=1535, 2006 HS Base Case	cont	load	125%	100%	%06>	125%	123%	112%	101%	101%	100%	%66	97%	97%	95%	93%	%06>	106%	~06>	%06>	108%
Case	rating	[MVA]	121.7	413.5	413.5	121.7	400	80	576	160	85.1	109	109	121	85.1	240	85.1	85.1	85.1	319	200
		D	1	-	~	-	-	~	~	~	~	-	~	~	~	~	~	-	-	- 	1
		-kv-	115	230	230	115	230	115	230	115	115	115	115	115	115	230	115	115	115	115	115
	TO	name	EFMORGTP	PAWNEE	PAWNEE	EFMORGTP	STEGALL	FMWEST	PAWNEE	BRUSHTAP	TIMNTHTP	ADENA	ADENA	FMWEST	SANDCRK	SIDNEYDC	"AULT "	"AULT "	COBBLKTP	BEAVERCK	BEAVERCK
		BUS #	73305	70311	70311	73305	73190	73379	70311	73031	73201	73464	73464	73379	73493	73181	73552	73552	73044	73020	73020
		ZONE	752	706	206	752	753	752	752	752	754	752	752	752	752	756	754	754	754	706	752
		-kv-	115	230	230	115	230	115	230	115	115	115	115	115	115	230	115	115	115	115	115
	FROM	name	BRUSHTAP	FTLUPTON	FTLUPTON	BRUSHTAP	ARCHER	BJOUTAP	STORY	BEAVERCK	COBBLKTP	BEAVERCK	НОҮТ	EFMORGTP	BRIGHTNW	SIDNEY	"NUNN"	<b>BLKHLWTP</b> "	BLKHLWTP	B.CK PS	B.CK TRI
		BUS#	73031	70192	70192	73031	73009	73023	73192	73020	73044	73020	73088	73305	73030	73180	73145	73024	73024	73013	73015

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	I	-kv-	115	115	230	230	230	115	115	115	230	115	230	230	115	230	
		name	ADENA	CHEYENNE	<b>BUCKLEY1</b>	SIDNEY	PLNENDSS	FMWEST	BEAVERCK	FMWEST	SMOKYHIL	ADENA	Weld LM	LINCOLNT	DERBY 1	WINDSOR	
	To	BUS #	73464	73043	70067	73180	70570	73379	73020	73379	70396	73464	73212	73531	70153	70474	
		-kv-	115	115	230	230	230	115	115	115	115	115	230	230	115	230	
	CONTINGENCY	name	BEAVERCK	ARCHER	SMOKYHIL	N.YUMA	LOOKOUT	EFMORGTP	B.CK PS	EFMORGTP	SMOKYHIL	BEAVERCK	WELD PS	MIDWAYBR	CHEROKEE	AULT	
	From	BUS #	73020	73008	70396	73143	70266	73305	73013	73305	70395	73020	70471	73413	70108	73011	
		Cnt #	245	221	153	379	118	514	234	514	621	245	567	524	37	568	
Base Case (6b-r1.sav) TOT 3=1470 TOT 7 = 592	cont	load	%06>	117%	114%	114%	108%	~06>	94%	~06>	106%	~06>	95%	~06>	111%	92%	
Base with 300 WW Wind Base With 300 WW Wind Base MW 75 = 51 MW TOT 7 = 621 MW	cont	load	%06>	118%	113%	112%	112%	110%	107%	107%	106%	~06>	98%	~06>	100%	95%	
300 MW  with 2 Paw-Ft. Lup 1ines TOT3=1455 MW, TOT2=525 MM, (06-fix-1'.sav)	cont	load	%06>	116%	114%	115%	115%	~06>	~06>	%06>	105%	%06>	~06>	%06>	102%	101%	
300 MW  with 2 Paw-Ft. Lup 11nes, TOT 3 = 1530 MW TOT7 = 572 MW, (06-fix.sav)	cont	load	64%	116%	117%	119%	116%	%06>	101%	%06>	105%	%06>	94%	%06>	104%	<06>	
Base with 300 WW Wind WM 7131 = 5 TOT MM 7131 = 570T TOT	cont	load	123%	119%	117%	116%	114%	110%	109%	108%	107%	105%	104%	104%	102%	102%	
1011=634 MM, (6b.sav) 101 3=1535, 2006 HS Base Case	cont	load	112%	117%	111%	118%	110%	%06>	%06>	%06>	101%	101%	100%	%06>	112%	97%	
Case	rating	[MVA]	80	80	434.6	167	280	109	224	109	168	160	495	121	135	500	
	I	Q	1	-	-	-	-	-	-	-	2	-	-	-	-	٢	
		-kv-	115	115	. 230	230	230	115	230	115	230	115	230	115	115	230	
	5	name	FMWEST	CROWCRK	MEADOWHL	SIDNEY	VALMONT	ADENA	<b>B.CK TRI</b>	ADENA	SMOKYHIL	BRUSHTAP	WINDSOR	FMWEST	DERBY 2	ST.VRAIN	
	I	BUS #	73379	73480	70283	73180	70447	73464	73016	73464	70396	73031	70474	73379	70154	70410	
		ZONE	752	753	200	756	703	752	752	752	200	752	754	752	200	206	
	1	-kv-	115	115	230	115	115	115	115	115	115	115	230	115	115	230	
	FROM	name	BIJOUTAP	CHEYENNE	SMOKYHIL	SIDNEY	VALMONT	BEAVERCK	<b>B.CK TRI</b>	НОҮТ	SMOKYHIL	BEAVERCK	AULT	EFMORGTP	CHEROKEE	WELD PS	
	1	BUS#	73023	73043	70396	73179	70444	73020	73015	73088	70395	73020	73011	73305	70108	70471	

								Case	2006 HS Base Case TOT 3=1535, TOT7=634 MW, (6b.sav)	bniW WM 300 briw عده WM ۲۸۵۱ TOT 3 = ۲۵۲۱ WW TOT 7 = ۵۲۵ WM (6د.sav)	300 MW with 2 Paw-Ft. Lup lines, TOT 3 = 1530 MW TOT7 = 572 MW, (06-fix.sav)	300 MW  with 2 Paw-Ft. Lup 1ines  TOT3=1455 MM, TOT7=525 MW, (06-fix-r1.sav)	briW WM 00£ fiw 9s88 WM 1541 = 5 TOT (vss.11-98) WM 158 = 7 TOT	Base Case (6b-r1.sav) TOT 3=1470 TOT 7 = 592							
	FROM				TO		2	ating	cont	cont	cont	cont	cont	cont		From	CONTINGENCY		To		
BUS#	name	¥	ZONE	BUS #	name	¥	<u>e</u>	WA]	load	load	load	load	load	load	Cnt #	BUS #	name	в Ż	# SN	-name	-kv-
73013	B.CK PS	115	706	73020	BEAVERCK	115	-	319	%06>	102%	%06>	%06>	%06>	%06>	129	70311	PAWNEE	230 7	0343	QUINCY :	230
70108	CHEROKEE	115	700	70153	DERBY 1	115	-	135	111%	101%	103%	101%	%66	109%	38	70108	CHEROKEE	115 7	0154 [	ERBY 2	115
73078	HARMONY	230	754	73199	TIMBERLN	230	1	172.1	%66	101%	%96	93%	97%	%96	567	70471	WELD PS	230 7	3212 V	/ELD LM	230
73145	NUNN	115	754	73552	AULT	115	-	85.1	107%	101%	91%	%06>	~06>	~06>	226	73009	ARCHER	230 7	3011	AULT	230
65425	DAVEJOHN	115	679	73071	GLENRCKS	115	-	109	101%	101%	92%	%66	100%	%66	560	65425	DAVEJOHN	115 7	.3070 GI	ENRCKN	115
73024	BLKHLWTP	115	754	73552	AULT	115	-	85.1	106%	101%	101%	%06>	~06>	~06>	226	73009	ARCHER	230 7	3011	AULT	230
73011	AULT	230	754	73212	WELD LM	230	2	142.2	98%	100%	94%	%06	95%	94%	231	73011	AULT	230 7	3212 V	/ELD LM	230
73011	AULT	230	754	73212	WELD LM	230	1	142.2	98%	100%	94%	%06	95%	94%	232	73011	AULT	230 7	3212 V	/ELD LM	230
70313	ORCHARD	230	200	70283	MEADOWHL	230	1	134.6	95%	100%	101%	97%	86%	92%	153	70396	SMOKYHIL	230 7	.0067 B	JCKLEY1	230
70191	FTLUPTON	115	706	70192	FTLUPTON	230	~	280	92%	100%	107%	105%	98%	91%	178	70447	VALMONT	230 7	0410 S	T.VRAIN	230
73104	LAGRANGE	115	753	73189	STEGALL	115	-	121.7	96%	100%	94%	%06>	~06>	92%	227	73009	ARCHER	230 7	3190 S	TEGALL	230
70192	FTLUPTON	230	706	70605	HENRYLAK	230	-	435	92%	%66	109%	107%	97%	91%	81	70192	FTLUPTON	230 7	0529 J	LGREEN	230
73113	LNGMNTNW	115	754	73133	MEADOW	115	-	110.2	100%	%66	102%	102%	%66	101%	360	73115	LONGPEAK	115 7	3196	TERRY	115
70354	RIDGE	115	200	70355	RIDGE	230	2	100	111%	98%	101%	104%	%66	111%	619	70354	RIDGE	115 7	0355	RIDGE	230
70610	REUNION	230	200	70047	BARRLAKE	230	1	134.6	%06	98%	100%	%66	66%	96%	82	70192	FTLUPTON	230 7	.0605 HI	ENRYLAK	230
70470	WELD PS	115	706	70471	WELD PS	230	2	150	%66	95%	101%	%06>	95%	98%	677	73211	WELD LM	115 7	3212 V	/ELD LM	230
70073	CALIFOR1	115	200	70299	NORTH542	115	-	150	107%	94%	~06~	98%	86%	%06>	27	70087	CAPHILL1	115 7	0215 H	ARRISPS	115
70605	HENRYLAK	230	706	70362	RIVERDAL	230	-	435	%06>	94%	104%	102%	92%	%06>	81	70192	FTLUPTON	230 7	0529 J	LGREEN	230
70087	CAPHILL1	115	200	70300	NORTH547	115	-	150	105%	91%	94%	94%	91%	%06>	23	70073	CALIFOR1	115 7	N 6620.	DRTH542	115
73013	B.CK PS	115	706	73020	BEAVERCK	115	-	319	101%	101%	101%	%66	~06>	%66	573	73192	STORY	230 7	0311 F	AWNEE	230
73020	BEAVERCK	115	752	73031	BRUSHTAP	115	-	160	<90%	<90%	101%	97%	%06>	~06~	575	73192	STORY	230 7	0311 F	AWNEE	230